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Titel CRITERIA FOR SIZING VENT SYSTEM
 KRIERIEN FÜR DIE GRÖSSE DES ENTLÜFTUNGSSYSTEMS
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CRITERIA FOR SIZING OF VENT SYSTEM
FOR LIQUEFIER SMART TB-LNG 140 TPD

REV. Rev.	DATA Date	DESCRIZIONE Description	COMPILATO Compiled	APPROVATO Approved
0A	22/05/2023	First issue	Zetti	Antonelli

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1 INTRODUCTION

This document covers:

1 – information related to the flow rate of the safety valves for thermal expansion of gas or evaporation of liquid in case of fire. The sizing of the safety valves orifice is not the subject of this document.

2 – definition of the flow rates vented in the various design cases.

The API 521 code is used for the definition of the discharge flow rates of the safety valves.

The reference documents are:

- Document No. I 20784 – 520REZH700001000SRI002 – Piping & Instrumentation Diagram
- Document No. 2220698-00-10-001/EST105701 – 520REZH598004003SRI001 – NG Treatment unit - Piping & Instrumentation Diagram

2 DISCHARGE FLOW RATE DEFINITION OF SAFETY VALVES FOR FIRE CASE

The discharge flow rates of the safety valves calculated for thermal expansion due to fire in the various sections of the plant are listed below.

plant inlet and liquefier section

PSV603 – 746 Nm³/h – 607 kg/h

PSV605 – 296 Nm³/h – 241 kg/h

PSV704 – 667 Nm³/h – 536 kg/h

PSV705 – 19 Nm³/h – 15 kg/h

PSV707 – 20 Nm³/h – 16 kg/h

PSV721 – 5 Nm³/h – 3 kg/h

PSV720 – 213 Nm³/h – 171 kg/h

PSV716 – 213 Nm³/h – 171 kg/h

Total flow rate: 2179 Nm³/h equal to 1760 kg/h with average M.W. of 18,1 kg/kmole

Regeneration gas and Boil-Off Gas section

PSV529 – 23 Nm³/h – 21 kg/h

PSV526 – 23 Nm³/h – 19 kg/h

PSV530 – 174 Nm³/h – 140 kg/h

PSV501 – 81 Nm³/h – 65 kg/h

PSV502 – 81 Nm³/h – 65 kg/h

PSV503 – 81 Nm³/h – 65 kg/h

PSV507 – 15 Nm³/h – 12 kg/h

PSV905 – 92 Nm³/h – 94 kg/h

PSV914 – 234 Nm³/h – 179 kg/h (note 1)

PSV915 – 242 Nm³/h – 248 kg/h

PSV913 – 152 Nm³/h – 155 kg/h

PSV901 – 81 Nm³/h – 65 kg/h

PSV902 – 81 Nm³/h – 65 kg/h

PSV903 – 81 Nm³/h – 65 kg/h

PSV907 – 15 Nm³/h – 12 kg/h

Total flow rate: 1456 Nm³/h equal to 1270 kg/h with average M.W. of 19,55 kg/kmole.

Note 1: the cold box zone and EW9000 heater surfaces are considered; the KO drum zone is not considered because located in a separate area and with a smaller surface.

Note 2: PSV1608 (on hot flare header) not considered because the hot flare is in a separate area.

Gas treatment section

PSV144 – 270 Nm³/h – 217 kg/h

PSV135 – 45 Nm³/h – 37 kg/h

PSV103 – 106 Nm³/h – 87 kg/h

PSV167 – 1204 Nm³/h – 967 kg/h

PSV129 – 1478 Nm³/h – 1187 kg/h

PSV117 – 747 Nm³/h – 618 kg/h

PSV489 – 997 Nm³/h – 801 kg/h

PSV422 – 405 Nm³/h – 326 kg/h

PSV436 – 997 Nm³/h – 801 kg/h

PSV437 – 997 Nm³/h – 801 kg/h

PSV451 – 114 Nm³/h – 92 kg/h

PSV465 – 155 Nm³/h – 124 kg/h

PSV482 – 191 Nm³/h – 153 kg/h

PSV478 – 248 Nm³/h – 199 kg/h

PSV484 – 51 Nm³/h – 41 kg/h

PSV419 – 358 Nm³/h – 288 kg/h

PSV421 – 127 Nm³/h – 102 kg/h

Total flow rate: 8490 Nm³/h equal to 6841 kg/h with average M.W. of 18,06 kg/kmole.

Storage and truck loading section

PSV1905A – 198 Nm³/h – 159 kg/h

PSV1907 – 12 Nm³/h – 13 kg/h

PSV1906 – 500 Nm³/h – 402 kg/h

PSV1904A – 87 Nm³/h – 70 kg/h

PSV1901A – 237 Nm³/h – 190 kg/h

PSV1AA – 1307 Nm³/h – 1051 kg/h (Note 1)

PSV8A – 3 Nm³/h – 2 kg/h

PSV1905B – 198 Nm³/h – 159 kg/h

PSV1904B – 87 Nm³/h – 70 kg/h

PSV1901B – 237 Nm³/h – 190 kg/h

PSV1BB – 1307 Nm³/h – 1051 kg/h (Note 1)

PSV8B – 3 Nm³/h – 2 kg/h
PSV1930A – 237 Nm³/h – 190 kg/h
PSV1932A – 69 Nm³/h – 56 kg/h
PSV1933A – 13 Nm³/h – 10 kg/h (Note 2)
PSV1940A – 69 Nm³/h – 56 kg/h
PSV1938A – 119 Nm³/h – 96 kg/h
PSV1930B – 237 Nm³/h – 190 kg/h
PSV1932B – 69 Nm³/h – 56 kg/h
PSV1933B – 13 Nm³/h – 10 kg/h (Note 2)
PSV1940B – 69 Nm³/h – 56 kg/h
PSV1938B – 119 Nm³/h – 96 kg/h
PSV1955A – 76 Nm³/h – 78 kg/h
PSV1956A – 119 Nm³/h – 96 kg/h
PSV1957A – 5 Nm³/h – 5 kg/h
PSV1958A – 5 Nm³/h – 5 kg/h
PSV1959A – 5 Nm³/h – 5 kg/h
PSV1954A – 74 Nm³/h – 76 kg/h
PSV1961A – 195 Nm³/h – 157 kg/h
PSV1950A – 119 Nm³/h – 96 kg/h
PSV1951A – 119 Nm³/h – 96 kg/h
PSV1952A – 119 Nm³/h – 96 kg/h
PSV1960A – 119 Nm³/h – 96 kg/h
PSV1977A – 8 Nm³/h – 9 kg/h
PSV1955B – 76 Nm³/h – 78 kg/h
PSV1956B – 119 Nm³/h – 96 kg/h
PSV1957B – 5 Nm³/h – 5 kg/h
PSV1958B – 5 Nm³/h – 5 kg/h
PSV1959B – 5 Nm³/h – 5 kg/h
PSV1954B – 74 Nm³/h – 76 kg/h
PSV1961B – 195 Nm³/h – 157 kg/h
PSV1950B – 119 Nm³/h – 96 kg/h
PSV1951B – 119 Nm³/h – 96 kg/h
PSV1952B – 119 Nm³/h – 96 kg/h
PSV1960B – 119 Nm³/h – 96 kg/h
PSV1977B – 8 Nm³/h – 9 kg/h

Total flow rate: 7116 Nm³/h equal to 5805 kg/h with average M.W. of 18,28 kg/kmole.

Note 1: only 1 PSV of LNG tanks is considered because each valve is designed for full capacity.

Note 2: only 1 PSV of LNG pumps is considered because each valve is designed for full capacity.

3 VENT FLOW RATE DEFINITION

For the definition of the flow rates to be vented, the following design cases were considered:

CASE 1: emergency condition due to fire in the production section

CASE 2: emergency plant shutdown

CASE 3: emergency vent from HV715 valve

CASE 4: emergency vent from PSV530 safety valve

CASE 5: emergency condition due to fire in the storage section

For each case, the calculation of the vent flow rate is described below.

CASE 1: emergency condition due to fire in the production section

The flow rate discharged in this condition is generated by all the safety valves discharge in the gas treatment + liquefaction + regeneration gas Boil-Off Gas management zone considering both the gas expansion and the vaporization of the LNG liquid due to the fire. The safety valves of the storage area (LNG tanks and loading bays) are not considered since the production area and the storage area are considered independent and not subject to a domino effect.

Based on what is indicated in the previous chapter 2, the vent flow rate for this case is the sum of the following flow rates:

Plant inlet section and liquefier: 1760 kg/h with average M.W. 18.1 kg/kmole

Regeneration gas section and Boil-Off Gas: 1270 kg/h with average M.W. 19.55 kg/kmole

Gas treatment section: 8490 Nm³/h equal to 6841 kg/h with average M.W. 18.06 kg/kmol

The total flow rate is therefore 9871 kg/h with average M.W. 18.26 kg/kmole at a temperature of +178 °C. The temperature is calculated on the basis of the temperature increase resulting from the pressure increase for the high pressure process circuit from the operating value up to the set value of the safety valves.

CASE 2: emergency plant shutdown

The vented flow rate in this condition is generated by the discharge of the LNG present in the cold box and of the natural gas present in the cold box and in the gas treatment plant (dryer section and absorption section) during emergency depressurization.

The discharge flow rate is calculated considering the depressurization sequence described below.

CASE 2.1: first step - drain of the LNG present in the cold box from the HV711 drain valve

- Volume of liquid present in the cold box: 0,88 m³

- Mass of liquid to be drained: 415 kg (density 471 kg/m³)

- Liquid pressure upstream the drain valve: 3 bara (liquid head included)

- Liquid pressure downstream the drain valves: 2 bara (discharge back pressure)

- Temperature: -159 / -166 °C

- Required time for drain: 2,5 minutes

To discharge the mass in 2,5 minutes the discharge flow rate is $415 \cdot 60 / 2,5 = 9960$ kg/h

The attachment 1 – case 1 shows the calculation of the HV711 valve

CASE 2.2: second step - depressurization in parallel of the liquefier section, the dryer section and the absorption section

A - Liquefier section depressurization

Depressurization always takes place by venting the gas from the HV711 valve

- Volume of gas to be vented: 1 m³ at a pressure of 43.5 bar upstream of the PV703 valve
- Depressurisation end pressure: 6 bara; at this pressure the introduction of nitrogen begins
- Gas temperature for mass calculation: 10°C, corresponding to the gas temperature upstream of the liquefier exchanger
- Pressure upstream of the HV711 valve (and downstream of the PV703 valve): is kept at 4 bara as the control of the PV703 valve is switched to the controller PIC715C
- Pressure downstream of the HV711 valve: 2 bara
- Temperature of the discharged gas: -134°C (the gas cools down as it passes through the liquefaction exchanger up to this temperature)
- Quantity of gas to be vented during depressurization from 43.5 bara to 6 bara: $1 \times (43,5-6) \times (273/283) \times (18.03/22,414) = 29,1$ kg

The following conditions shall be verified:

- a – the PV703 valve can discharge the mass within an acceptable time frame (not exceeding 10 minutes).
- b – the PV703 and HV711 valves can discharge the mass in the 1st minute in order to reduce the pressure to 33 bara.

a – check that the PV703 valve can discharge the mass within an acceptable time frame to reduce the pressure from 43.5 bara to 6 bara

- The gas flow rate that the HV711 valve can discharge when 100% opened is 2900 kg/h (see attachment 2 – case 2)
- The PV703 valve, 100% opened, can discharge 2803 kg/h, value given by interpolation between the flow rate of 2900 kg/h with an inlet pressure of 45 bara (attachment 4 - case 1) and 2575 kg/h with inlet pressure of 40 bara (attachment 7 – case 3)
- The reduction of flow rate discharged by the PV703 valve 100% opened as the inlet pressure decreases is indicated below:
 - inlet pressure 45 bara: 2900 kg/h attachment 4 – case 1)
 - inlet pressure 40 bara: 2575 kg/h attachment 7 – case 3)
 - inlet pressure 35 bara: 2250 kg/h attachment 7 – case 1)
 - inlet pressure 30 bara: 1927 kg/h attachment 6 – case 3)
 - inlet pressure 25 bara: 1605 kg/h attachment 6 – case 2)
 - inlet pressure 20 bara: 1285 kg/h attachment 6 – case 1)

inlet pressure 15 bara: 965 kg/h attachment 5 – case 3)

inlet pressure 10 bara: 630 kg/h attachment 5 – case 2)

inlet pressure 6 bara: 326 kg/h attachment 5 – case 1)

- Interpolating between the above values, the flow rate calculated as the inlet pressure to the PV703 valve decreases by every 1 bar is equal to: $1 \text{ m}^3 \times (1) \text{ bar} \times (273/283) \times (18,03/22,414) = 0,776 \text{ kg/bar}$. With this value the time corresponding to each pressure reduction of 1 bar is then calculated. Attachment 9 shows the calculation of the time required to reduce the pressure from 43,5 bar to 6 bar. As a demonstration, the calculation of the first pressure reduction step from 43,5 to 42 bara (Deltap=1,5 bar) is shown below:
 $(0,776 \text{ kg/bar} \times 1,5 \text{ bar}) / ((2803 \text{ kg/h} + 2705 \text{ kg/h})/2) \times 60 \text{ min/h} = 0,025 \text{ min}$.
The time required to depressurize the liquefier section up to 6 bara is 1,5 minutes.
- Therefore the total time for LNG drainage and liquefier section depressurization is 4 minutes.

b – check that the PV703 and HV711 valves can discharge the mass in the 1st minute in order to reduce the pressure from 43,5 to 33 bara

- The mass to be discharged in the 1st minute is $1 \text{ m}^3 \times (43,5-33) \text{ bara} \times (273/283) \times (18,03/22,414) \times 60 \text{ min/h} = 525 \text{ kg/h}$.

From attachment 2 - case 1 it is verified that the HV711 valve can discharge this flow rate.

From attachment 4 - case 3 it is verified that the PV703 valve can discharge this flow rate of 525 kg/h even at the minimum pressure of 33 bara with opening less than 100%.

B - Depressurization of the dryer section

Depressurization takes place by venting the gas from the HV705 valve (ON_OFF ball valve) and limiting the flow with the FO708 orifice.

- Volume of gas to be vented: 3,5 m³ starting from a pressure of 44 bara and considering 2 pressurized dryer vessels: worst case condition with one vessel in operation and one vessel at the beginning of depressurization.
- Depressurisation end pressure: 6 bara; at this pressure the introduction of nitrogen begins.
- Pressure downstream of the orifice: 2 bara
- Average temperature of the gas to be vented: 20°C
- Quantity of gas to be vented: $3,5 \text{ m}^3 \times (44-6) \text{ bara} \times (273/293) \times (18,06/22,414) = 100 \text{ kg}$
With the 15,5 mm orifice diameter, 6 bara are reached after 260 seconds (4 minutes and 20 sec) and the flow rate at the beginning (maximum flow rate) is equal to 0,94 kg/sec (3384 kg/h).
Furthermore, the 33 barA are reached after 38 sec. (less than 1 minute).

Attachment 10 shows the calculation of the depressurization.

Note: if only one vessel has to be depressurised (the vessel in operation) the volume is 2,2 m³ instead of 3,5 m³ and the pressure of 6 bara is reached after 160 seconds and the pressure of 33 bara after 22 seconds.

C - Absorption section depressurization

Depressurization takes place by venting the gas from the HV764 valve (ON_OFF ball valve) and limiting the flow rate with the RO169 orifice.

- Volume of gas to be vented: 7,2 m3 starting from a pressure of 44 bara
 - Depressurisation end pressure: 6 bara; at this pressure the introduction of nitrogen begins
 - Pressure downstream of the orifice: 2 bara
 - Average temperature of the gas to be vented: 40°C
 - Quantity of gas to be vented: $7,2 \text{ m}^3 \times (44-6) \text{ bara} \times (273/313) \times (18,06/22,414) = 192 \text{ kg}$
- With the 17.3 mm orifice diameter, 6 bara are reached after 405 seconds (6 minutes and 45 sec.) and the flow rate at the beginning (maximum flow rate) is equal to 1,123 kg/sec (4043 kg/h).

Furthermore, 33 bara are reached after 60 sec (1 minute)

Attachment 11 shows the calculation of the depressurization

In summary, the vent conditions for emergency depressurization are:

- Capacity: $2900 + 3384 + 4043 = 10327 \text{ kg/h}$
- Temperature: $(2900 \times (-134) + 3384 \times 20 + 4043 \times 40) / 10327 = -15.1^\circ\text{C}$
- Molecular weight: $(2900 \times 18,03 + 3384 \times 18,06 + 4043 \times 18,06) / 10327 = 18,05 \text{ kg/kmole}$

CASE 3: emergency vent from HV715 valve

The emergency condition considered in this case is the one corresponding to the failure of the J/T PV703 valve fully opened and in the conservative hypothesis that the liquefaction exchanger can liquefy and subcool the entire flow rate (condition of maximum flowing mass). The HV715 valve with HIC715 controller set at 5 barg protects the system from opening of the safety valve PSV705 set at 5 barg. Attachment 8 - case 2 shows the calculation sheet of the PV703 valve 100% open with the fluid at operating conditions:

- inlet pressure 43,15 bara
- outlet pressure 5 bar
- inlet temperature -168 / -159 °C
- liquid density: 457,97 kg/h

The maximum flow rate is 10900 kg/h.

Attachment 3 - case 1 shows the calculation sheet for the HV715 valve venting such flow rate with an inlet pressure of 5 bara and an outlet pressure of 2 bara.

CASE 4: emergency vent from PSV530 safety valve

The emergency condition considered in this case is the one corresponding to the spurious opening of the regeneration valve of the absorber vessel in operation.

The flow rate discharged from the spurious opening of the regeneration valve in operation is limited by the calibrated orifice FO530 and is equal to 6717 kg/h (1,866 kg/sec) at a temperature of 20°C.

This flow rate is obtained by sizing the diameter of the FO530 orifice based on the maximum acceptable pressure drop of 0,3 bar with the nominal regeneration flow rate. The PSV530 is in any case sized to discharge the entire flow rate of 6717 kg/h.

Attachment 12 shows the calculation of the FO530 orifice.

CASE 5: emergency condition due to fire in the storage section

The vented flow rate in this condition is generated by the discharge of all the safety valves of the storage and tank loading area considering both the gas expansion and the vaporization of the LNG liquid due to the fire.

Considering what is indicated in chapter 2, the flow rate at the vent in this case is 5805 kg/h with M.W. 18,28 kg/kmole and temperature -138,65 °C, equilibrium temperature of the evaporating LNG at a pressure of 6 bara (set pressure of the PSVs of the LNG tank which act first).

4 ATTACHMENT

Attachment 1: HV711 valve calculation sheet – case 1

Attachment 2: HV711 valve calculation sheet – case 1 and case 2

Attachment 3: HV715 valve calculation sheet – case 1

Attachment 4: PV703 valve calculation sheet – case 1 and case 3

Attachment 5: PV703 valve calculation sheet – case 1, case 2 and case 3

Attachment 6: PV703 valve calculation sheet – case 1, case 2 and case 3

Attachment 7: PV703 valve calculation sheet – case 1 and case 3

Attachment 8: PV703 valve calculation sheet – case 2

Attachment 9: Liquefier Depressurization Time Calculation Sheet

Attachment 10: FO708 orifice depressurization calculation spreadsheet

Attachment 11: RO169 orifice depressurization calculation spreadsheet

Attachment 12: FO530 orifice depressurization calculation spreadsheet

ATTACHMENT 1

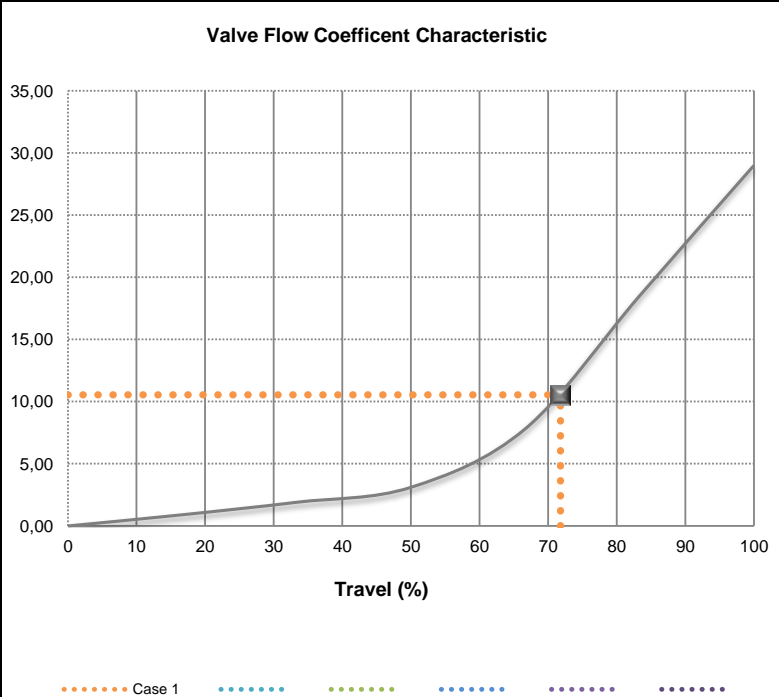
OMC		OMC Calculation Sheet			Filled By		
					Date	18/05/2023	
					Vmech 3.9.5		
1	Quotation No.	Rev.			Project		
2	Customer				End User		
3	RFQ No.				Location		
4	Item	Item			PED (2014/68/CE) Category		B + C2
5		Quantity	1		NACE		Not required
6		Tag No.	HV 711		Piping diam. – Schedule		3" - Schedules 40
7		Service			Min Ambient / Medium Temp.		20 C / 20 C
8		Valve Type	Globe single seat		Design Press. / Temp.		
9		Medium / State	LNG		Liquid		
10	Process Data		Units	Case 1	Case 2		
11		Density	kg/m3	470,880			
12		Viscosity	cP	0,120			
13		Flow rate	kg/h	9960,000			
14		Inlet pressure	bar.a	3,000			
15		Outlet pressure	bar.a	2,000			
16		DP	bar.a	1,000			
17		Temperature	C	-166,530			
18	Results and Factors	Remarks					
19		Calculated	Cv	16,780			
20		Selected	Cv	50			
21		Travel	%	68,3			
22		SPL @ 1m	Db	58,770			
23		Velocity on inlet line	m/s	1,232			
24	Velocity on outlet line	m/s	1,232				
25	Valve Model	KA10	KA12-15-2"-AP28-3/15		Valve Function	Control	
26	Body / Bonnet	Inlet/Outlet Size	2"		Valve Flow Coefficient Characteristic 		
27		Inlet/Outlet conn.	ANSI 150 SW				
28		Body Material	ASME SA-351 CF8M				
29		Body Gasket	ARMED GRAPHITE				
30		Studs	ASME SA-193 B8M				
31		Nuts	ASME SA-194 GM				
32		Bonnet type	EXTENDED				
33		Bonnet Material	ASTM A182 F316				
34	Balancing System	Not Required					
35	Trim	Cv	50				
36		Seat Type	Threaded				
37		Seat material	ASTM A182 F316				
38		Seat size	49,0 mm				
39		Flow action	To Open				
40		Stem Material	VIRGIN PTFE				
41		Flow Divider	NO				
42		Flow Divider Material	-				
43		Plug Characteristic	EQP				
44		Plug (Mat.)	ASTM A182 F316				
45	Seal Type / Material	SOFT/VIRGIN PTFE					
46	Leakage Class	VI					
47	Leakage Standard	EN60534-4 / ANSI FCI					
48	Packing	Type	ECOPACK1				
49		Material	GRAPHITE				
50	Actuator	Actuator type	AP28		Remarks		
51		Air failure	Open				
52		Stroke (mm)	20				
53		Actuator Signal (Psi)	3/15				
54		Shutoff pressure	-				
55		Spring case/Yoke	Carbon Steel				
56		Diaphragm material	NBR				
57		Handwheel	NO				
58	Spring Action	Normally open					
59	Notes						Page 1/1

ATTACHMENT 2

		OMC Calculation Sheet			Filled By		
					Date	18/05/2023	
1	Quotation No.	Rev.			Project		
2	Customer				End User		
3	RFQ No.				Location		
4	Item	Item			PED (2014/68/CE) Category		B + C2
5		Quantity	1		NACE		Not required
6		Tag No.	HV 711_		Piping diam. - Schedule		3" - Schedules 40
7		Service			Min Ambient / Medium Temp.		20 C / 20 C
8		Valve Type	Globe single seat		Design Press. / Temp.		
9		Medium / State	LNG		Gas	Molecular weight 18,03	
10	Process Data		Units	Case 1	Case 2		
11		Density	kg/m3	4,420	4,420		
12		Viscosity	cP	0,001	0,001		
13		Flow rate	kg/h	525,000	2899,955		
14		Inlet pressure	bar.a	4,000	4,000		
15		Outlet pressure	bar.a	2,000	2,000		
16		DP	bar.a	2,000	2,000		
17	Temperature	C	-134,000	-134,000			
18	Results and Factors	Remarks					
19		Calculated	Cv	8,583	50,000		
20		Selected	Cv	50	50		
21		Travel	%	56,1	100,0		
22		SPL @ 1m	Db	75,081	78,410		
23		Velocity on inlet line	m/s	6,919	38,219		
24	Velocity on outlet line	m/s	9,812	54,199			
25	Valve Model	KA10	KA12-15-2"-AP28-3/15		Valve Function	Control	
26	Body / Bonnet	Inlet/Outlet Size	2"				
27		Inlet/Outlet conn.	ANSI 150 SW				
28		Body Material	ASME SA-351 CF8M				
29		Body Gasket	ARMED GRAPHITE				
30		Studs	ASME SA-193 B8M				
31		Nuts	ASME SA-194 GM				
32		Bonnet type	EXTENDED				
33	Bonnet Material	ASTM A182 F316					
34	Balancing System	Not Required					
35	Trim	Cv	50				
36		Seat Type	Threaded				
37		Seat material	ASTM A182 F316				
38		Seat size	49,0 mm				
39		Flow action	To Open				
40		Stem Material	VIRGIN PTFE				
41		Flow Divider	NO				
42		Flow Divider Material	-				
43		Plug Characteristic	EQP				
44		Plug (Mat.)	ASTM A182 F316				
45	Seal Type / Material	SOFT/VIRGIN PTFE					
46	Leakage Class	VI					
47	Leakage Standard	EN60534-4 / ANSI FCI					
48	Packing	Type	ECOPACK1				
49		Material	GRAPHITE				
50	Actuator	Actuator type	AP28		Remarks		
51		Air failure	Open				
52		Stroke (mm)	20				
53		Actuator Signal (Psi)	3/15				
54		Shutoff pressure	-				
55		Spring case/Yoke	Carbon Steel				
56		Diaphragm material	NBR				
57		Handwheel	NO				
58	Spring Action	Normally open					
59	Notes						Page 1/1

ATTACHMENT 3

		<h2 style="margin: 0;">OMC Calculation Sheet</h2>		Filled By		
				Date	18/05/2023	
				Vmech 3.9.5		
1	Quotation No.	Rev.		Project		
2	Customer			End User		
3	RFQ No.			Location		
4	Item	Item	3		PED (2014/68/CE) Category	
5		Quantity	1		NACE	
6		Tag No.	HV 715		Piping diam. – Schedule	
7		Service			Min Ambient / Medium Temp.	
8		Valve Type	Globe single seat		Design Press. / Temp.	
9		Medium / State	LNG		Liquid	
10	Process Data		Units	Case 1		
11		Density	kg/m3	475,970		
12		Viscosity	cP	0,120		
13		Flow rate	kg/h	10900,000		
14		Inlet pressure	bar.a	5,000		
15		Outlet pressure	bar.a	2,000		
16		DP	bar.a	3,000		
17		Temperature	C	-168,000		
18	Results and Factors	Remarks				
19		Calculated	Cv	10,545		
20		Selected	Cv	29		
21		Travel	%	71,8		
22		SPL @ 1m	Db	66,929		
23		Velocity on inlet line	m/s	1,334		
24		Velocity on outlet line	m/s	1,334		
25	Valve Model	KA10	KA12-15-2"-AP34-15/60		Valve Function	Control
26	Body / Bonnet	Inlet/Outlet Size	2"			
27		Inlet/Outlet conn.	ANSI 150 SW			
28		Body Material	ASME SA-351 CF8M			
29		Body Gasket	ARMED GRAPHITE			
30		Studs	ASME SA-193 B8M			
31		Nuts	ASME SA-194 GM			
32		Bonnet type	EXTENDED			
33		Bonnet Material	ASTM A182 F316			
34	Balancing System	Not Required				
35	Trim	Cv	29			
36		Seat Type	Threaded			
37		Seat material	ASTM A182 F316			
38		Seat size	38,0 mm			
39		Flow action	To Open			
40		Stem Material	316 S.S. STL.GR.6			
41		Flow Divider	NO			
42		Flow Divider Material	-			
43		Plug Characteristic	EQP			
44		Plug (Mat.)	ASTM A182 F316			
45	Seal Type / Material	METALLIC/316 S.S. STL.GR.6				
46	Leakage Class	V				
47	Leakage Standard	EN60534-4 / ANSI FCI				
48	Packing	Type	LP200			
49		Material	VIRGIN PTFE			
50	Actuator	Actuator type	AP34			
51		Air failure	Close			
52		Stroke (mm)	20			
53		Actuator Signal (Psi)	15/60			
54		Shutoff pressure	9,013 bar.a			
55		Spring case/Yoke	Carbon Steel			
56		Diaphragm material	NBR			
57		Handwheel	NO			
58		Spring Action	Normally close			
59	Notes					Page 1/1



SAMSON CALCULATION SHEET



L43374

1	Customer	SIAD MACCHINE IMPIANTI				Tag No.	PV 703				
2	Project No.	L43374				Item	3	Qty.	1	Status	
3	Unit					Quot. No.	161087539		Revision	0	
4	PID					Order No.					
5	Line No.	LNG-101-2"-C27-N / LNG-102-2"-A27-N				Date	22.05.2023				
6	PROCESS DATA										
7	Service	Throttling				Medium	Natural Gas				
8	Phase	gas				Medium Cust.					
9			Unit		Case 1		Case 2		Case 3		
10	Flow Rate	W	kg/h		2900				525		
11	Inlet Pressure	p1	bar(a)		45				33		
12	Outlet Pressure	p2	bar(a)		4				4		
13	Inlet Temperature	T1	°C		-134				-134		
14	Inlet molecular Weight	M	g/mol		18,03				18,03		
15	Vapor Pressure	pv	bar(a)								
16	Critical Pressure	pc	bar(a)								
17	Ratio of Specific Heats	γ	-		1,37				1,37		
18	Compressibility	Z	-		0,869				0,971		
19	Inlet Viscosity	η	mPas		0,0101				0,00887		
20	Outlet Vapor Content	xd2	%								
21	Outlet Vapor Density	pv2	kg/m³								
22	Flow Conditions	-	-								
23	RESULTS AND FACTORS										
24	Min Required Size	d	mm		43				18,3		
25	Outlet Velocity	w	Mach		0,447				0,0752		
26	Valve Coeff. Calculated	Cv	-		3,01				0,775		
27	Relative Travel	T	%		100				64,8		
28	SPL (SAMSON Standard values)	LA	dB (A)		94				81		
29	Differential Pressure Ratio	xF x	-		0,91				0,88		
30	FL Value	FL	-		0,96				0,98		
31	xFmr/xT Value	xFmr xT	-		0,79				0,81		
32	Valve Style Factor	Fd	-		0,48				0,41		
33	xFz Value at Load	xFz	-								
34	Level Exponent	F1 G1	-		-3,86				-4,06		
35	Slope Exponent	F2 G2	-		1,55				1,5		
36	Correction Term	DLf	dB								
37	DESIGN					77	LINE				
38	Shut-Off Pressure Min	0 bar(g)	Max	52 bar(g)	78	Size / Rating / Pipe Class					
39	t1max		Max	-168 °C	79	In NPS 2" / Schedule 10S /					
40	Supply Pressure Min	4,2 bar(g)	Max	10 bar(g)	80	Out NPS 2" / Schedule 10S /					
41	Pressure Min	bar(g)	Max	bar(g)	81	Pipe Inner Dia. / Wallthickness 54,8 mm / 2,8 mm					
42	Temperature Min	°C	Max	°C	82	Insu. none					
43	Ambient Temp. Min	-25 °C	Max	40 °C	83	ACTUATOR					
44	VALVE BODY / BONNET					84	Manufacturer / Type SAMSON / 3277				
45	Manufacturer / Type	SAMSON / 3248			85	Size 355 cm²					
46	Style	Globe Globe valve			86	Fail Action Fail close					
47	Nominal Size	NPS 1 1/2			87	Bench/Oper. Range 1.9 to 3.3 bar/2,95 ... 3,65 bar					
48	Rating	Class 600			88	Actuator Body Mat. 1.0976 / 1.0982					
49	Body Material	A351 CF8			89	Actuator Style Pneumatic					
50	Connection In/Out	Welding ends			90	Stroke Limit. -					
51	Connection In/Out	SWE, ASME B16.34/B16.5			91	Membrane Material NBR					
52	Bonnet Type	Bellows			92	Handwheel -					
53	Bellow Material	316Ti			93	Set Point / -Range /					
54	Packing Material	PTFE			94	ACTUATOR RESULTS					
55	Packing Type	Standard			95	Safety Factor	Open	12,1	Close	1,66	
56	Body Gasket	-			96	Req. Act. Force 6,31 kN					
57	Flow Direction	FTO			97	Max. Act. Force Fmax 45 kN					
58	NACE				98	Max. dp Dpmax 90,58 bar					
59	TRIM					99	Min. Press. Act. ps0req 1,95 bar				
60	Valve Coefficient	Cv 3			100	Req. Dp Dps 0,05 bar					
61	Rated Travel	15 mm			101	Req. Dp Dpst100-0 bar					
62	Seat Bore	24 mm			102	Actuator Force Fa 10,47 kN					
63	Stem Ø	16 mm			103	Min. required Supply 3,85 bar(g)					
64	Characteristic	Equal perc.			104	Max. allowable Supply 6 bar(g)					
65	Noise Reduction	-			105	ATTENUATION PLATES					
66	Balanced	-			106	Type					
67	Plug Facing	Metal			107	Size In / Out					
68	Plug Material	R30016			108	Rating					
69	Stem Material	A479 316/A479 316L			109	Plates Material				Qty.	
70	Seat Facing	Stellited			110	REMARKS					
71	Seat Material	A182 F316/A182 F316L			111						
72	Cage Material				112						
73	Flow Divider Mat.				113						
74	Leakage Class	IV			114						
75	Rev.	Date	Description	Prpd.	Chd.						App.
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SAMSON CALCULATION SHEET



L43374

1	Customer	SIAD MACCHINE IMPIANTI				Tag No.	PV 703				
2	Project No.	L43374				Item	3	Qty.	1	Status	
3	Unit					Quot. No.	161087539		Revision	0	
4	PID					Order No.			Date	22.05.2023	
5	Line No.	LNG-101-2"-C27-N / LNG-102-2"-A27-N									
6	PROCESS DATA										
7	Service	Throttling				Medium	Natural Gas				
8	Phase	gas				Medium Cust.					
9			Unit		Case 1	Case 2	Case 3				
10	Flow Rate	W	kg/h		326	630	965				
11	Inlet Pressure	p1	bar(a)		6	10	15				
12	Outlet Pressure	p2	bar(a)		4	4	4				
13	Inlet Temperature	T1	°C		-134	-134	-134				
14	Inlet molecular Weight	M	g/mol		18,03	18,03	18,03				
15	Vapor Pressure	pv	bar(a)								
16	Critical Pressure	pc	bar(a)								
17	Ratio of Specific Heats	γ	-		1,37	1,37	1,37				
18	Compressibility	Z	-		0,869	0,869	0,869				
19	Inlet Viscosity	η	mPas		0,0101	0,0101	0,0101				
20	Outlet Vapor Content	xd2	%								
21	Outlet Vapor Density	pv2	kg/m³								
22	Flow Conditions	-	-								
23	RESULTS AND FACTORS										
24	Min Required Size	d	mm		14,4	20	24,8				
25	Outlet Velocity	w	Mach		0,0468	0,0905	0,139				
26	Valve Coeff. Calculated	Cv	-		3	3	3				
27	Relative Travel	T	%		100	100	100				
28	SPL(SAMSON Standard values)	LA	dB (A)		62	75	81				
29	Differential Pressure Ratio	xF x	-		0,33	0,6	0,73				
30	FL Value	FL	-		0,96	0,96	0,96				
31	xFmr/xT Value	xFmr xT	-		0,79	0,79	0,79				
32	Valve Style Factor	Fd	-		0,48	0,48	0,48				
33	xFz Value at Load	xFz	-								
34	Level Exponent	F1 G1	-		-3,86	-3,86	-3,86				
35	Slope Exponent	F2 G2	-		1,5	1,5	1,5				
36	Correction Term	DLf	dB								
37	DESIGN					77	LINE				
38	Shut-Off Pressure Min	0 bar(g)	Max	52 bar(g)	78	Size / Rating / Pipe Class					
39	t1max		Max	-168 °C	79	In NPS 2" / Schedule 10S /					
40	Supply Pressure Min	4,2 bar(g)	Max	10 bar(g)	80	Out NPS 2" / Schedule 10S /					
41	Pressure Min	bar(g)	Max	bar(g)	81	Pipe Inner Dia. / Wallthickness 54,8 mm / 2,8 mm					
42	Temperature Min	°C	Max	°C	82	Insu. none					
43	Ambient Temp. Min	-25 °C	Max	40 °C	83	ACTUATOR					
44	VALVE BODY / BONNET					84	Manufacturer / Type SAMSON / 3277				
45	Manufacturer / Type	SAMSON / 3248			85	Size 355 cm²					
46	Style	Globe Globe valve			86	Fail Action Fail close					
47	Nominal Size	NPS 1 1/2			87	Bench/Oper. Range 1.9 to 3.3 bar/2,95 ... 3,65 bar					
48	Rating	Class 600			88	Actuator Body Mat. 1.0976 / 1.0982					
49	Body Material	A351 CF8			89	Actuator Style Pneumatic					
50	Connection In/Out	Welding ends			90	Stroke Limit. -					
51	Connection In/Out	SWE, ASME B16.34/B16.5			91	Membrane Material NBR					
52	Bonnet Type	Bellows			92	Handwheel -					
53	Bellow Material	316Ti			93	Set Point / -Range /					
54	Packing Material	PTFE			94	ACTUATOR RESULTS					
55	Packing Type	Standard			95	Safety Factor	Open	12,1	Close	1,66	
56	Body Gasket	-			96	Req. Act. Force 6,31 kN					
57	Flow Direction	FTO			97	Max. Act. Force Fmax 45 kN					
58	NACE				98	Max. dp Dpmax 90,58 bar					
59	TRIM					99	Min. Press. Act. ps0req 1,95 bar				
60	Valve Coefficient	Cv 3			100	Req. Dp Dps 0,05 bar					
61	Rated Travel	15 mm			101	Req. Dp Dpst100-0 bar					
62	Seat Bore	24 mm			102	Actuator Force Fa 10,47 kN					
63	Stem Ø	16 mm			103	Min. required Supply 3,85 bar(g)					
64	Characteristic	Equal perc.			104	Max. allowable Supply 6 bar(g)					
65	Noise Reduction	-			105	ATTENUATION PLATES					
66	Balanced	-			106	Type					
67	Plug Facing	Metal			107	Size In / Out					
68	Plug Material	R30016			108	Rating					
69	Stem Material	A479 316/A479 316L			109	Plates Material				Qty.	
70	Seat Facing	Stellited			110	REMARKS					
71	Seat Material	A182 F316/A182 F316L			111						
72	Cage Material				112						
73	Flow Divider Mat.				113						
74	Leakage Class	IV			114						
75	Rev.	Date	Description	Prpd.	Chd.	App.					
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SAMSON CALCULATION SHEET



L43374

1	Customer	SIAD MACCHINE IMPIANTI			Tag No.	PV 703				
2	Project No.	L43374			Item	3	Qty.	1		
3	Unit				Quot. No.	161087539		Status		
4	PID				Order No.			Revision		
5	Line No.	LNG-101-2"-C27-N / LNG-102-2"-A27-N			Date	22.05.2023				
6	PROCESS DATA									
7	Service	Throttling			Medium	Natural Gas				
8	Phase	gas			Medium Cust.					
9			Unit	Case 1	Case 2	Case 3				
10	Flow Rate	W	kg/h	1285	1605	1927				
11	Inlet Pressure	p1	bar(a)	20	25	30				
12	Outlet Pressure	p2	bar(a)	4	4	4				
13	Inlet Temperature	T1	°C	-134	-134	-134				
14	Inlet molecular Weight	M	g/mol	18,03	18,03	18,03				
15	Vapor Pressure	pv	bar(a)							
16	Critical Pressure	pc	bar(a)							
17	Ratio of Specific Heats	γ	-	1,37	1,37	1,37				
18	Compressibility	Z	-	0,869	0,869	0,869				
19	Inlet Viscosity	η	mPas	0,0101	0,0101	0,0101				
20	Outlet Vapor Content	xd2	%							
21	Outlet Vapor Density	pv2	kg/m³							
22	Flow Conditions	-	-							
23	RESULTS AND FACTORS									
24	Min Required Size	d	mm	28,6	32	35,1				
25	Outlet Velocity	w	Mach	0,188	0,233	0,282				
26	Valve Coeff. Calculated	Cv	-	3	3	3				
27	Relative Travel	T	%	100	100	100				
28	SPL(SAMSON Standard values)	LA	dB (A)	84	87	89				
29	Differential Pressure Ratio	xF x	-	0,8	0,84	0,87				
30	FL Value	FL	-	0,96	0,96	0,96				
31	xFmr/xT Value	xFmr xT	-	0,79	0,79	0,79				
32	Valve Style Factor	Fd	-	0,48	0,48	0,48				
33	xFz Value at Load	xFz	-							
34	Level Exponent	F1 G1	-	-3,86	-3,86	-3,86				
35	Slope Exponent	F2 G2	-	1,5	1,5	1,51				
36	Correction Term	DLf	dB							
37	DESIGN				77	LINE				
38	Shut-Off Pressure Min	0 bar(g)	Max	52 bar(g)	78	Size / Rating / Pipe Class				
39	t1max		Max	-168 °C	79	In NPS 2" / Schedule 10S /				
40	Supply Pressure Min	4,2 bar(g)	Max	10 bar(g)	80	Out NPS 2" / Schedule 10S /				
41	Pressure Min	bar(g)	Max	bar(g)	81	Pipe Inner Dia. / Wallthickness 54,8 mm / 2,8 mm				
42	Temperature Min	°C	Max	°C	82	Insu. none				
43	Ambient Temp. Min	-25 °C	Max	40 °C	83	ACTUATOR				
44	VALVE BODY / BONNET				84	Manufacturer / Type SAMSON / 3277				
45	Manufacturer / Type	SAMSON / 3248			85	Size 355 cm²				
46	Style	Globe Globe valve			86	Fail Action Fail close				
47	Nominal Size	NPS 1 1/2			87	Bench/Oper. Range 1.9 to 3.3 bar/2,95 ... 3,65 bar				
48	Rating	Class 600			88	Actuator Body Mat. 1.0976 / 1.0982				
49	Body Material	A351 CF8			89	Actuator Style Pneumatic				
50	Connection In/Out	Welding ends			90	Stroke Limit. -				
51	Connection In/Out	SWE, ASME B16.34/B16.5			91	Membrane Material NBR				
52	Bonnet Type	Bellows			92	Handwheel -				
53	Bellow Material	316Ti			93	Set Point / -Range /				
54	Packing Material	PTFE			94	ACTUATOR RESULTS				
55	Packing Type	Standard			95	Safety Factor	Open	12,1	Close	1,66
56	Body Gasket	-			96	Req. Act. Force 6,31 kN				
57	Flow Direction	FTO			97	Max. Act. Force Fmax 45 kN				
58	NACE				98	Max. dp Dpmax 90,58 bar				
59	TRIM				99	Min. Press. Act. ps0req 1,95 bar				
60	Valve Coefficient	Cv 3			100	Req. Dp Dps 0,05 bar				
61	Rated Travel	15 mm			101	Req. Dp Dpst100-0 bar				
62	Seat Bore	24 mm			102	Actuator Force Fa 10,47 kN				
63	Stem Ø	16 mm			103	Min. required Supply 3,85 bar(g)				
64	Characteristic	Equal perc.			104	Max. allowable Supply 6 bar(g)				
65	Noise Reduction	-			105	ATTENUATION PLATES				
66	Balanced	-			106	Type				
67	Plug Facing	Metal			107	Size In / Out				
68	Plug Material	R30016			108	Rating				
69	Stem Material	A479 316/A479 316L			109	Plates Material Qty.				
70	Seat Facing	Stellited			110	REMARKS				
71	Seat Material	A182 F316/A182 F316L			111					
72	Cage Material				112					
73	Flow Divider Mat.				113					
74	Leakage Class	IV			114					
75	Rev.	Date	Description	Prpd.	Chd.	App.				
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SAMSON CALCULATION SHEET



L43374

1	Customer	SIAD MACCHINE IMPIANTI				Tag No.	PV 703				
2	Project No.	L43374				Item	3	Qty.	1	Status	
3	Unit					Quot. No.	161087539		Revision	0	
4	PID					Order No.					
5	Line No.	LNG-101-2"-C27-N / LNG-102-2"-A27-N				Date	22.05.2023				
6	PROCESS DATA										
7	Service	Throttling				Medium	Natural Gas				
8	Phase	gas				Medium Cust.					
9			Unit		Case 1		Case 2		Case 3		
10	Flow Rate	W	kg/h		2250				2575		
11	Inlet Pressure	p1	bar(a)		35				40		
12	Outlet Pressure	p2	bar(a)		4				4		
13	Inlet Temperature	T1	°C		-134				-134		
14	Inlet molecular Weight	M	g/mol		18,03				18,03		
15	Vapor Pressure	pv	bar(a)								
16	Critical Pressure	pc	bar(a)								
17	Ratio of Specific Heats	γ	-		1,37				1,37		
18	Compressibility	Z	-		0,869				0,869		
19	Inlet Viscosity	η	mPas		0,0101				0,0101		
20	Outlet Vapor Content	xd2	%								
21	Outlet Vapor Density	pv2	kg/m³								
22	Flow Conditions	-	-								
23	RESULTS AND FACTORS										
24	Min Required Size	d	mm		37,9				40,5		
25	Outlet Velocity	w	Mach		0,332				0,387		
26	Valve Coeff. Calculated	Cv	-		3				3		
27	Relative Travel	T	%		100				100		
28	SPL(SAMSON Standard values)	LA	dB (A)		91				92		
29	Differential Pressure Ratio	xF x	-		0,89				0,9		
30	FL Value	FL	-		0,96				0,96		
31	xFmr/xT Value	xFmr xT	-		0,79				0,79		
32	Valve Style Factor	Fd	-		0,48				0,48		
33	xFz Value at Load	xFz	-								
34	Level Exponent	F1 G1	-		-3,86				-3,86		
35	Slope Exponent	F2 G2	-		1,52				1,53		
36	Correction Term	DLf	dB								
37	DESIGN					77	LINE				
38	Shut-Off Pressure Min	0 bar(g)	Max	52 bar(g)	78	Size / Rating / Pipe Class					
39	t1max		Max	-168 °C	79	In NPS 2" / Schedule 10S /					
40	Supply Pressure Min	4,2 bar(g)	Max	10 bar(g)	80	Out NPS 2" / Schedule 10S /					
41	Pressure Min	bar(g)	Max	bar(g)	81	Pipe Inner Dia. / Wallthickness 54,8 mm / 2,8 mm					
42	Temperature Min	°C	Max	°C	82	Insu. none					
43	Ambient Temp. Min	-25 °C	Max	40 °C	83	ACTUATOR					
44	VALVE BODY / BONNET					84	Manufacturer / Type SAMSON / 3277				
45	Manufacturer / Type	SAMSON / 3248			85	Size 355 cm²					
46	Style	Globe Globe valve			86	Fail Action Fail close					
47	Nominal Size	NPS 1 1/2			87	Bench/Oper. Range 1.9 to 3.3 bar/2,95 ... 3,65 bar					
48	Rating	Class 600			88	Actuator Body Mat. 1.0976 / 1.0982					
49	Body Material	A351 CF8			89	Actuator Style Pneumatic					
50	Connection In/Out	Welding ends			90	Stroke Limit. -					
51	Connection In/Out	SWE, ASME B16.34/B16.5			91	Membrane Material NBR					
52	Bonnet Type	Bellows			92	Handwheel -					
53	Bellow Material	316Ti			93	Set Point / -Range /					
54	Packing Material	PTFE			94	ACTUATOR RESULTS					
55	Packing Type	Standard			95	Safety Factor	Open	12,1	Close	1,66	
56	Body Gasket	-			96	Req. Act. Force 6,31 kN					
57	Flow Direction	FTO			97	Max. Act. Force Fmax 45 kN					
58	NACE				98	Max. dp Dpmax 90,58 bar					
59	TRIM					99	Min. Press. Act. ps0req 1,95 bar				
60	Valve Coefficient	Cv 3			100	Req. Dp Dps 0,05 bar					
61	Rated Travel	15 mm			101	Req. Dp Dpst100-0 bar					
62	Seat Bore	24 mm			102	Actuator Force Fa 10,47 kN					
63	Stem Ø	16 mm			103	Min. required Supply 3,85 bar(g)					
64	Characteristic	Equal perc.			104	Max. allowable Supply 6 bar(g)					
65	Noise Reduction	-			105	ATTENUATION PLATES					
66	Balanced	-			106	Type					
67	Plug Facing	Metal			107	Size In / Out					
68	Plug Material	R30016			108	Rating					
69	Stem Material	A479 316/A479 316L			109	Plates Material Qty.					
70	Seat Facing	Stellited			110	REMARKS					
71	Seat Material	A182 F316/A182 F316L			111						
72	Cage Material				112						
73	Flow Divider Mat.				113						
74	Leakage Class	IV			114						
75	Rev.	Date	Description	Prpd.	Chd.	App.	115				
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SIAD MACCHINE IMPIANTI		SAMSON CALCULATION SHEET				samson		
L43374								
1	Customer	SIAD MACCHINE IMPIANTI				Tag No.		PV 703
2	Project No.	L43374				Item		3 Qty. 1 Status
3	Unit					Quot. No.		161087539 Revision 0
4	PID					Order No.		Date 22.05.2023
5	Line No.	LNG-101-2"-C27-N / LNG-102-2"-A27-N						
PROCESS DATA								
7	Service	Throttling			Medium			Natural Gas
8	Phase	liquid			Medium Cust.			
9			Unit	Case 1	Case 2	Case 3		
10	Flow Rate	W	kg/h		10900			
11	Inlet Pressure	p1	bar(a)		43,15			
12	Outlet Pressure	p2	bar(a)		5			
13	Inlet Temperature	T1	°C		-168			
14	Inlet Density	rho1	kg/m³		475,97			
15	Vapor Pressure	pv	bar(a)		3,61			
16	Critical Pressure	pc	bar(a)		46			
17	Ratio of Specific Heats	γ	-					
18	Compressibility	Z	-					
19	Inlet Viscosity	η	mPas		0,069			
20	Outlet Vapor Content	xd2	%					
21	Outlet Vapor mol. Weight	pv2	g/mol					
22	Flow Conditions	-	-				Critical cavitation	
RESULTS AND FACTORS								
24	Min Required Size	d	mm		40,2			
25	Outlet Velocity	w	m/s		5,06			
26	Valve Coeff. Calculated	Cv	-		3			
27	Relative Travel	T	%		100			
28	SPL(SAMSON Standard values)	LA	dB (A)		79			
29	Differential Pressure Ratio	xF x	-		0,96			
30	FL Value	FL	-		0,96			
31	xFmr/xT Value	xFmr xT	-		0,7			
32	Valve Style Factor	Fd	-		0,48			
33	xFz Value at Load	xFz	-		0,53			
34	Level Exponent	F1 G1	-		-7,14			
35	Slope Exponent	F2 G2	-		0,3			
36	Correction Term	DLf	dB		4,06			
37	DESIGN				77	LINE		
38	Shut-Off Pressure Min	0 bar(g)	Max	52 bar(g)	78	Size / Rating / Pipe Class		
39	t1max		Max	-168 °C	79	In NPS 2" / Schedule 10S /		
40	Supply Pressure Min	4,2 bar(g)	Max	10 bar(g)	80	Out NPS 2" / Schedule 10S /		
41	Pressure Min	bar(g)	Max	bar(g)	81	Pipe Inner Dia. / Wallthickness 54,8 mm / 2,8 mm		
42	Temperature Min	°C	Max	°C	82	Insu. none		
43	Ambient Temp. Min	-25 °C	Max	40 °C	83	ACTUATOR		
44	VALVE BODY / BONNET				84	Manufacturer / Type SAMSON / 3277		
45	Manufacturer / Type	SAMSON / 3248			85	Size 355 cm²		
46	Style	Globe Globe valve			86	Fail Action Fail close		
47	Nominal Size	NPS 1 1/2			87	Bench/Oper. Range 1.9 to 3.3 bar/2,95 ... 3,65 bar		
48	Rating	Class 600			88	Actuator Body Mat. 1.0976 / 1.0982		
49	Body Material	A351 CF8			89	Actuator Style Pneumatic		
50	Connection In/Out	Welding ends			90	Stroke Limit. -		
51	Connection In/Out	SWE, ASME B16.34/B16.5			91	Membrane Material NBR		
52	Bonnet Type	Bellows			92	Handwheel -		
53	Bellow Material	316Ti			93	Set Point / -Range /		
54	Packing Material	PTFE			94	ACTUATOR RESULTS		
55	Packing Type	Standard			95	Safety Factor	Open 12,1 Close 1,66	
56	Body Gasket	-			96	Req. Act. Force	6,31 kN	
57	Flow Direction	FTO			97	Max. Act. Force	Fmax 45 kN	
58	NACE				98	Max. dp	Dpmax 90,58 bar	
59	TRIM				99	Min. Press. Act.	ps0req 1,95 bar	
60	Valve Coefficient	Cv 3			100	Req. Dp	Dps 0,05 bar	
61	Rated Travel	15 mm			101	Req. Dp	Dpst100-0 bar	
62	Seat Bore	24 mm			102	Actuator Force	Fa 10,47 kN	
63	Stem Ø	16 mm			103	Min. required Supply	3,85 bar(g)	
64	Characteristic	Equal perc.			104	Max. allowable Supply	6 bar(g)	
65	Noise Reduction	-			105	ATTENUATION PLATES		
66	Balanced	-			106	Type		
67	Plug Facing	Metal			107	Size In / Out		
68	Plug Material	R30016			108	Rating		
69	Stem Material	A479 316/A479 316L			109	Plates Material	Qty.	
70	Seat Facing	Stellited			110	REMARKS		
71	Seat Material	A182 F316/A182 F316L			111			
72	Cage Material				112			
73	Flow Divider Mat.				113			
74	Leakage Class	IV			114			
75	Rev.	Date	Description	Prpd.	Chd.	App.		
76	0	22.05.2023		zanabo				

ATTACHMENT 9

Calculation of depressurization time for cold box

Calculation of flow rate of valve PV703 at following conditions:

relative travel %	100
gas temperature °C	-134
outlet pressure bara	4

Inlet

pressure flow rate

bara	kg/h	
45	2900	from supplier calculation
44	2835	interpolation
43.5	2803	interpolation
43	2770	interpolation
42	2705	interpolation
41	2640	interpolation
40	2575	from supplier calculation
39	2510	interpolation
38	2445	interpolation
37	2380	interpolation
36	2315	interpolation
35	2250	from supplier calculation
34	2185	interpolation
33	2121	interpolation
32	2056	interpolation
31	1992	interpolation
30	1927	from supplier calculation
29	1863	interpolation
28	1798	interpolation
27	1734	interpolation
26	1669	interpolation
25	1605	from supplier calculation
24	1541	interpolation
23	1477	interpolation
22	1413	interpolation
21	1349	interpolation
20	1285	from supplier calculation
19	1221	interpolation
18	1157	interpolation
17	1093	interpolation
16	1029	interpolation
15	965	from supplier calculation
14	898	interpolation
13	831	interpolation
12	764	interpolation
11	697	interpolation
10	630	from supplier calculation
9	554	interpolation
8	478	interpolation
7	402	interpolation
6	326	from supplier calculation

volume of gas to be vented m³
 gas temperature °C
 gas molecular weight kg/kmole

1
10
18.03

Calculation of depressurization time for each 1 bar pressure reduction:

step number	starting pressure		vented mass M1 kg	PV703 flow rate		time of step min
	P1 bara	P2 bara		rate at P1 Q1 kg/h	rate at P2 Q2 kg/h	
1	43.5	42	1.164	2803	2705	0.025
2	42	41	0.776	2705	2640	0.017
3	41	40	0.776	2640	2575	0.018
4	40	39	0.776	2575	2510	0.018
5	39	38	0.776	2510	2445	0.019
6	38	37	0.776	2445	2380	0.019
7	37	36	0.776	2380	2315	0.020
8	36	35	0.776	2315	2250	0.020
9	35	34	0.776	2250	2185.4	0.021
10	34	33	0.776	2185.4	2120.8	0.022
11	33	32	0.776	2120.8	2056.2	0.022
12	32	31	0.776	2056.2	1991.6	0.023
13	31	30	0.776	1991.6	1927	0.024
14	30	29	0.776	1927	1862.6	0.025
15	29	28	0.776	1862.6	1798.2	0.025
16	28	27	0.776	1798.2	1733.8	0.026
17	27	26	0.776	1733.8	1669.4	0.027
18	26	25	0.776	1669.4	1605	0.028
19	25	24	0.776	1605	1541	0.030
20	24	23	0.776	1541	1477	0.031
21	23	22	0.776	1477	1413	0.032
22	22	21	0.776	1413	1349	0.034
23	21	20	0.776	1349	1285	0.035
24	20	19	0.776	1285	1221	0.037
25	19	18	0.776	1221	1157	0.039
26	18	17	0.776	1157	1093	0.041
27	17	16	0.776	1093	1029	0.044
28	16	15	0.776	1029	965	0.047
29	15	14	0.776	965	898	0.050
30	14	13	0.776	898	831	0.054
31	13	12	0.776	831	764	0.058
32	12	11	0.776	764	697	0.064
33	11	10	0.776	697	630	0.070
34	10	9	0.776	630	554	0.079
35	9	8	0.776	554	478	0.090
36	8	7	0.776	478	402	0.106
37	7	6	0.776	402	326	0.128

Gas depressurization time (min)	1.470
Time for liquid drain (min)	2.5
Total drain and depressurization time (min)	3.970

44	10	440	27	139144	2.92	critic	1.000	1.65	0.12	0.993	0.133	0.133	26	26	5.1	5.1	17.8	17.8	139145	139145	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
45	10	450	26	139145	2.78	critic	1.000	1.65	0.11	0.993	0.126	0.126	24	24	4.8	4.8	16.9	16.9	139146	139146	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
46	10	460	24	139146	2.64	critic	1.000	1.65	0.11	0.994	0.120	0.120	23	23	4.6	4.6	16.1	16.1	139147	139147	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
47	10	470	23	139147	2.51	critic	1.000	1.65	0.10	0.994	0.114	0.114	22	22	4.4	4.4	15.3	15.3	139149	139149	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
48	10	480	22	139149	2.39	critic	1.000	1.65	0.10	0.994	0.109	0.109	21	21	4.2	4.2	14.5	14.5	139150	139150	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
49	10	490	21	139150	2.27	critic	1.000	1.65	0.09	0.995	0.103	0.103	20	20	4.0	4.0	13.8	13.8	139151	139151	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
50	10	500	20	139151	2.16	critic	1.000	1.65	0.09	0.995	0.098	0.098	19	19	3.8	3.8	13.1	13.1	139152	139152	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
51	10	510	19	139152	2.05	critic	1.000	1.65	0.08	0.995	0.093	0.093	18	18	3.6	3.6	12.5	12.5	139153	139153	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
52	10	520	18	139153	1.95	subcritical	0.999	1.65	0.08	0.995	0.089	0.089	17	17	3.4	3.4	11.9	11.9	139154	139154	40.0	0.997	2.0	2.0	433.2	17.4	17.4	2.01	0.044	1.65
53	10	530	17	139154	1.85	subcritical	0.996	1.65	0.07	0.996	0.084	0.084	16	16	3.2	3.2	11.2	11.2	139154	139154	40.0	0.997	2.0	2.0	433.2	17.3	17.3	2.01	0.044	1.65
54	10	540	16	139154	1.76	subcritical	0.987	1.65	0.07	0.996	0.079	0.079	15	15	3.1	3.1	10.6	10.6	139155	139155	40.0	0.997	2.0	2.0	433.2	17.2	17.2	2.01	0.044	1.65
55	10	550	15	139155	1.68	subcritical	0.973	1.65	0.07	0.996	0.074	0.074	15	15	2.9	2.9	9.9	9.9	139156	139156	40.0	0.997	2.0	2.0	433.2	16.9	16.9	2.01	0.044	1.65
56	10	560	15	139156	1.60	subcritical	0.954	1.65	0.06	0.996	0.069	0.069	14	14	2.8	2.8	9.3	9.3	139157	139157	40.0	0.997	2.0	2.0	433.2	16.6	16.6	2.01	0.044	1.65
57	10	570	14	139157	1.52	subcritical	0.927	1.65	0.06	0.996	0.064	0.064	13	13	2.7	2.7	8.6	8.6	139157	139157	40.0	0.997	2.0	2.0	433.2	16.1	16.1	2.01	0.044	1.65
58	10	580	13	139157	1.45	subcritical	0.893	1.65	0.06	0.997	0.059	0.059	13	13	2.5	2.5	7.9	7.9	139158	139158	40.0	0.997	2.0	2.0	433.2	15.5	15.5	2.01	0.044	1.65
59	10	590	13	139158	1.39	subcritical	0.850	1.65	0.06	0.997	0.054	0.054	12	12	2.4	2.4	7.2	7.2	139158	139158	40.0	0.997	2.0	2.0	433.2	14.7	14.7	2.01	0.044	1.65
60	10	600	12	139158	1.33	subcritical	0.797	1.65	0.05	0.997	0.048	0.048	12	12	2.3	2.3	6.4	6.4	139159	139159	40.0	0.997	2.0	2.0	433.2	13.7	13.7	2.01	0.044	1.65
61	10	610	12	139159	1.28	subcritical	0.735	1.65	0.05	0.997	0.043	0.043	11	11	2.3	2.3	5.7	5.7	139159	139159	40.0	0.997	2.0	2.0	433.2	12.6	12.6	2.01	0.044	1.65
62	10	620	11	139159	1.23	subcritical	0.661	1.65	0.05	0.997	0.037	0.037	11	11	2.2	2.2	4.9	4.9	139160	139160	40.0	0.997	2.0	2.0	433.2	11.3	11.3	2.01	0.044	1.65
63	10	630	11	139160	1.19	subcritical	0.576	1.65	0.05	0.997	0.031	0.031	11	11	2.1	2.1	4.2	4.2	139160	139160	40.0	0.997	2.0	2.0	433.2	9.8	9.8	2.01	0.044	1.65
64	10	640	11	139160	1.16	subcritical	0.480	1.65	0.05	0.997	0.025	0.025	10	10	2.1	2.1	3.4	3.4	139160	139160	40.0	0.997	2.0	2.0	433.2	8.1	8.1	2.01	0.044	1.65
65	10	650	10	139160	1.13	subcritical	0.370	1.65	0.04	0.997	0.019	0.019	10	10	2.0	2.0	2.5	2.5	139160	139160	40.0	0.997	2.0	2.0	433.2	6.2	6.2	2.01	0.044	1.65
66	10	660	10	139160	1.11	subcritical	0.246	1.65	0.04	0.997	0.012	0.012	10	10	2.0	2.0	1.7	1.7	139161	139161	40.0	0.997	2.0	2.0	433.2	4.1	4.1	2.01	0.044	1.65
67	10	670	10	139161	1.09	subcritical	0.083	1.65	0.04	0.997	0.004	0.004	10	10	2.0	2.0	0.6	0.6	139161	139161	40.0	0.997	2.0	2.0	433.2	1.4	1.4	2.01	0.044	1.65

ATTACHMENT 12

Calculation of FO530

Flow rate through orifices (gas) - Perry ref - eq. 10.20		
orifice Ø	mm	21
Pipe internal Ø	mm	82.9
Pinlet	BarA	43.4
Poutlet	BarA	8
Molecular weight	kg/kmole	18.03
Temperature	°C	20
Coefficient cp/cv	-	1.34
Critical pressure ratio rc	-	0.5386
Pressure ratio r	-	0.1843
Check sonic/subsonic flow	-	SONIC
Compressibility factor	-	0.9
Factorβ (orifice Ø/pipe internal Ø)	-	0.25
Coefficient of Expansion Y	-	0.7496
Density ρ	kg/m³	35.680
Dynamic viscosity	cpoise	0.0170
Velocity in the orifice	m/sec	150.99
Reynolds number		6654730
Discharge Coefficient C	-	0.60
ΔP used in the calculation	Pascal	2002470
Orifice passage area A	m²	0.0003464
$Q = 3600 * Y * C * A * \sqrt{\frac{2 * \Delta P / \rho}{1 - (\beta^4)}}$	m³/h	188.26
	kg/h	6717.24
	kg/sec	1.866
	Nm³/h	8350.54